

# MECHANICS – Problem Set 3, distributed 2/22/22, due 3/8/22.

These problems provide practice with basic concepts of 3D nonlinear elasticity, and explore various reductions including balloons, elastic membranes, and compressible flow. Problem 1 is perhaps the richest (so don't leave it to the last minute).

(1) Consider a spherical rubber balloon (such as you might buy in a toy store). To a reasonable approximation we may:

- consider the reference domain to be a thin spherical annulus  $\Omega = \{x : r_0 - \epsilon < |X| < r_0 + \epsilon\}$ ;
- consider the air pressure in the balloon to be a constant  $p$ ;
- ignore the atmospheric pressure outside the balloon;
- consider experiments that are volume-controlled (fixing the volume of the interior of the balloon) or pressure-controlled (fixing the air pressure in the balloon).

From common experience, it is difficult to start blowing up a balloon, but then it gets easier, though eventually as the balloon gets large the blowing gets hard again (unless it bursts). This suggests a pressure-volume relation of the type shown in figure 1 below.

- (a) Assume the rubber is hyperelastic. Show that variational principle associated with a pressure-controlled experiment involves the energy  $E = \int_{\Omega} W(F) dX - p(\text{volume inside balloon})$ . (In other words, check that this gives the correct equilibrium and boundary conditions.) What variational principle is associated with a volume-controlled experiment?
- (b) Consider the limit  $\epsilon \rightarrow 0$  and assume the deformation is uniform expansion (i.e. the sphere  $X = r_0$  is mapped by  $x(X) = \lambda X$  to a sphere of radius  $\lambda r_0$ ). Suppose the rubber is isotropic and incompressible, so  $W$  has the form  $\Phi(\lambda_1, \lambda_2, \lambda_3)$  where  $\lambda_1, \lambda_2$ , and  $\lambda_3$  are the principal stretches (eigenvalues of  $(F^T F)^{1/2}$ ), which must satisfy  $\lambda_1 \lambda_2 \lambda_3 = 1$ . Show that when restricted to the case of “uniform expansion” the pressure-controlled variational principle takes the form  $E(\lambda) = c_1 F(\lambda) - c_2 p \lambda^3$  with

$$F(\lambda) = \Phi(\lambda, \lambda, \lambda^{-2}).$$

What are the constants  $c_1$  and  $c_2$ ?

- (c) Two commonly-used constitutive laws for rubber are the *neo-Hookean* energy

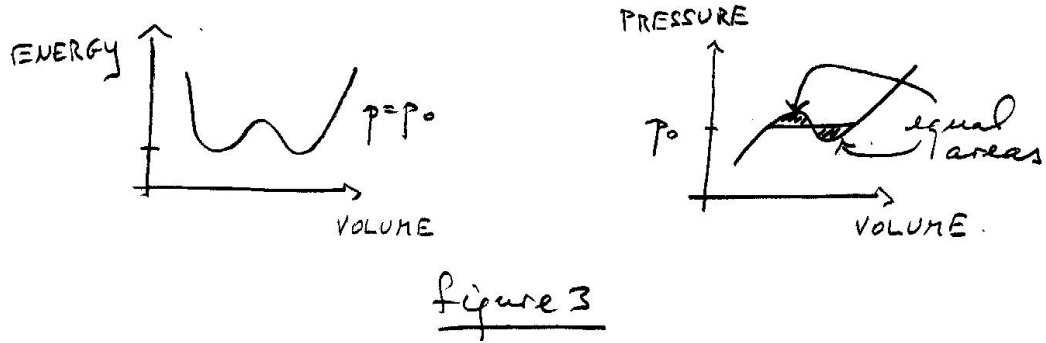
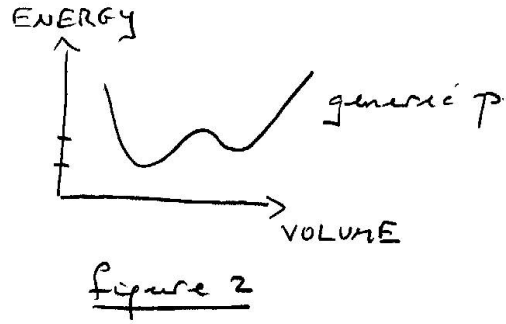
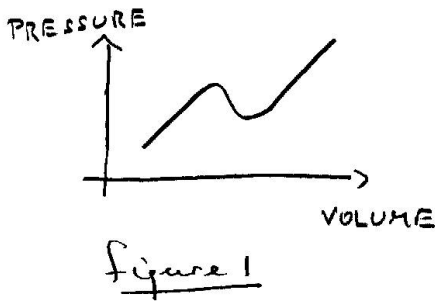
$$\Phi(\lambda_1, \lambda_2, \lambda_3) = a(\lambda_1^2 + \lambda_2^2 + \lambda_3^2 - 3)$$

with  $a > 0$ , and the *Mooney-Rivlin* energy

$$\Phi(\lambda_1, \lambda_2, \lambda_3) = a(\lambda_1^2 + \lambda_2^2 + \lambda_3^2 - 3) + (a/K)(\lambda_1^{-2} + \lambda_2^{-2} + \lambda_3^{-2} - 3)$$

with  $a > 0$  and  $K > 0$  (typically  $4 < K < 8$ ). Are these laws consistent with the nonmonotone pressure-volume relation shown in figure 1?

- (d) Let's think about the 1D energy  $E(\lambda)$ , using the non-monotonicity of the pressure-volume relation (as shown in Figure 1) but not using any special formula for  $F$  (such as those in part c). Evidently, certain values of the pressure  $p$  are consistent with 3 different volumes rather than just one. For such  $p$ ,  $E$  must have “double-well” structure, as shown in Figure 2. Show that the two wells have exactly the same depth precisely when  $p = p_0$  satisfies the “equal area rule” sketched in Figure 3.



(e) In real pressure-controlled experiments, as  $p$  crosses the value  $p_0$ , the balloon size changes (relatively suddenly) so that the volume occupies the deeper well (the energetically preferred state). How can this be reconciled with our 1D model?

(2) A homogeneous *elastic fluid* is a hyperelastic material with an energy function  $W(F) = h(\det F)$ . Show that the Cauchy stress is then  $\tau = -p(\rho)I$ , where  $p(\rho) = -h'(\rho_R/\rho)$ . [Here  $\rho_R$  is the density in Lagrangian, assumed constant, and  $\rho$  is the density in Eulerian variables.] Show that in this case the equations of elastodynamics are precisely the compressible Euler equations

$$\rho \left( \frac{\partial v}{\partial t} + v \cdot \nabla v \right) = -\nabla p(\rho) + \rho f$$

$$\frac{\partial \rho}{\partial t} + \sum \frac{\partial}{\partial x_i} (\rho v_i) = 0 .$$

[Note: to calculate  $\partial W / \partial F_{i\alpha}$  when  $W(F) = h(\det F)$  you'll to use Cramer's Rule, which says that  $\frac{\partial(\det F)}{\partial F} = (\det F)(F^T)^{-1}$ .]

(3) Consider a hyperelastic material, whose Piola-Kirchhoff stress tensor is given by  $P_{i\alpha} = \partial W / \partial F_{\alpha}^i$ .

(a) Show that if  $W$  is frame-indifferent (i.e. if  $W(F) = W(RF)$  for all orientation-preserving rotations  $R$ ) then the associated Cauchy stress  $\tau$  satisfies  $\tau(RF) = R\tau(F)R^T$ .

(b) Show that if  $W$  is isotropic (i.e. if it is frame indifferent and also  $W(FR) = W(F)$  for all orientation-preserving rotations  $R$ ) then the associated Cauchy stress  $\tau$  satisfies  $\tau(FR) = \tau(F)$ .

(4) Consider a homogeneous, isotropic, hyperelastic material with energy function  $W(F) = \psi(I_1, I_2, I_3)$ , where  $I_1, I_2, I_3$  are the elementary symmetric functions of  $B = FF^T$  ( $I_1 = \text{tr } B$ ,  $I_2 = \frac{1}{2}[(\text{tr } B)^2 - \text{tr}(B^2)]$ ,  $I_3 = \det B$ ). Show that the associated Cauchy stress has the form  $\tau = \phi_0 I + \phi_1 B + \phi_2 B^2$  with

$$\begin{aligned}\phi_0 &= 2 \frac{\partial \psi}{\partial I_3} \det F \\ \phi_1 &= 2 \frac{\partial \psi}{\partial I_1} (\det F)^{-1} + 2 \frac{\partial \psi}{\partial I_2} (\text{tr } B) (\det F)^{-1} \\ \phi_2 &= -2 \frac{\partial \psi}{\partial I_2} (\det F)^{-1} .\end{aligned}$$

(5) Rubber is typically modelled as a homogeneous, isotropic, *incompressible* hyperelastic material. The energy function for such a material has the form  $W(F) = \psi(I_1, I_2)$ , since all deformations must satisfy the constraint  $\det F = 1$ . Its Cauchy stress has the form  $\tau = -pI + \phi_1 B + \phi_2 B^2$ , where  $\phi_1, \phi_2$  have the form derived in Problem 4. Let's explore how  $W$  can be determined experimentally, using relatively simple experiments on thin membranes.

Consider a sheet (in reference coordinates) of length  $2A$ , width  $2B$ , and thickness  $2h$ , with  $A, B \gg h$ . Consider deformations of the form

$$x_i = \lambda_i X_i, \quad i = 1, 2, 3,$$

which can be maintained by edge tractions alone (i.e. for which the the faces  $X_3 = \pm h$  are traction-free). Show that

$$\begin{aligned}I_1 &= \lambda_1^2 + \lambda_2^2 + \frac{1}{\lambda_1^2 \lambda_2^2} \\ I_2 &= \frac{1}{\lambda_1^2} + \frac{1}{\lambda_2^2} + \lambda_1^2 \lambda_2^2\end{aligned}$$

and that the Cauchy stress is

$$\begin{aligned}\tau_{11} &= 2(\lambda_1^2 - \frac{1}{\lambda_1^2 \lambda_2^2}) (\frac{\partial \psi}{\partial I_1} + \lambda_2^2 \frac{\partial \psi}{\partial I_2}) \\ \tau_{22} &= 2(\lambda_2^2 - \frac{1}{\lambda_1^2 \lambda_2^2}) (\frac{\partial \psi}{\partial I_1} + \lambda_1^2 \frac{\partial \psi}{\partial I_2}) \\ \tau_{33} &= 0 \\ \tau_{ij} &= 0 \quad i \neq j .\end{aligned}$$

Conclude that  $\frac{\partial \psi}{\partial I_1}$  and  $\frac{\partial \psi}{\partial I_2}$  satisfy

$$\begin{aligned}\frac{\partial \psi}{\partial I_1} &= \frac{1}{2(\lambda_1^2 - \lambda_2^2)} \left( \frac{\lambda_1^2 \tau_{11}}{\lambda_1^2 - 1/\lambda_1^2 \lambda_2^2} - \frac{\lambda_2^2 \tau_{22}}{\lambda_2^2 - 1/\lambda_1^2 \lambda_2^2} \right) \\ \frac{\partial \psi}{\partial I_2} &= \frac{-1}{2(\lambda_1^2 - \lambda_2^2)} \left( \frac{\tau_{11}}{\lambda_1^2 - 1/\lambda_1^2 \lambda_2^2} - \frac{\tau_{22}}{\lambda_2^2 - 1/\lambda_1^2 \lambda_2^2} \right) .\end{aligned}$$

Thus by measuring the dependence of  $\tau_{11}$  and  $\tau_{22}$  on  $\lambda_1$  and  $\lambda_2$  one can determine the function  $\psi$ .