

Mechanics - Lecture 5 - 2/22/2022

[We'll start by finishing The Lecture 4 notes.]

We turn now to constitutive laws for nonlinear elasticity.

Two viewpoints are possible:

(a) "hyperelasticity": assume there's an underlying var'l principle, in other words specify the Piola-Kirchhoff stress

$$P_{ix} = \frac{\partial}{\partial F_{ix}} W(X, F)$$

where W = "elastic energy density" at reference pt X and def gradient F .

[This is the viewpoint introduced in Lecture 4.]

(b) "Cauchy elasticity": specify Cauchy stress $\tau = \hat{\tau}(X, F)$ as a fn of reference position X and def gradient F

Often a body might be homogeneous; then $W = W(F)$ & $\hat{\tau} \equiv \hat{\tau}(F)$.

Clearly (b) is more general than (a). [In a

hyperelastic material there is a rule of the form (b); but not every $\hat{\mathbb{E}}$ comes from an elastic energy [this will be easier to see when we get to linear elasticity].]

There are settings where the "Cauchy elastic" viewpoint is needed (see recent papers by Vincenzo + others on "odd elasticity".) But here I'll stick to the hyperelastic setting.

We always require "frame indifference". For hyperelasticity, this says

$$(*) \quad W(RF) = W(F) \quad \text{for any orientation-preserving rotation } R$$

For Cauchy elasticity, it says

$$(**) \quad \hat{\mathbb{E}}(RF) = R \hat{\mathbb{E}}(F) R^T \quad \text{for any orientation-preserving rotation } R.$$

[You'll be asked on HW3 to check that when $\hat{\mathbb{E}}$ comes from a frame-indifferent W it does satisfy (**).]

Interpretation of (*) : rotation does no elastic work; interp. of (**): an observer in a rotated coord system sees the same basic stress-strain law.

Let's check that when the Piola-Kirchhoff stress comes from an elastic energy

$$P_{i\alpha} = \frac{\partial W}{\partial F_{i\alpha}} \quad \text{with } W \text{ frame-indifferent}$$

the associated Cauchy stress $\mathbb{T}$ is at least symmetric. In fact, recalling that

$$P = J \mathbb{T} (F^{-1})^T \quad (\text{so } \mathbb{T} = J^{-1} P F^T)$$

with $J = \det F$, our task is to show that

$$\text{Frame indifference of } W \Rightarrow P F^T = \sum_{\alpha} P_{i\alpha} F_{i\alpha} \mathbf{e}_{\alpha} \mathbf{e}_{\alpha}^T \text{ is symmetric,}$$

For any skew-symmetric matrix Ω_{ij} . There's a rotation-valued curve $R(t)$ st $R(0) = \mathbb{I}$ and $\dot{R}(0) = \Omega$. Frame indifference gives

5.4

$$0 = \frac{d}{dt} \bigg|_{t=0} W(R(t)F) = \sum_{i,j} P_{ij}(F) (\dot{R}F)_{ij}$$

$$= \sum_{i,j} P_{ij}(F) \Omega_{ij} F_{ij}$$

So $P(F)F^T$ is orthogonal to the space of skew-symmetric matrices. So it is symmetric.

Many materials are isotropic. In hyperelasticity

$$\text{isotropy} \Leftrightarrow W(F) = W(FR) \text{ for any rotn } R.$$

$$\Leftrightarrow W(F) = \varphi(\lambda_1, \lambda_2, \lambda_3) \text{ where } \{\lambda_i\} \text{ are the principal stretches and } \varphi \text{ is a symmetric function of its arguments}$$

Corresp assertion for Cauchy elasticity:

$$\text{isotropy} \Leftrightarrow \hat{\mathbb{L}}(FR) = \hat{\mathbb{L}}(R) \text{ for any rotn } R.$$

There are some structural requirements that an elastic energy should satisfy. The most basic is that

- a) eqns of elastostatics are elliptic (and eqns of elastodynamics are hyperbolic).

A somewhat stronger condition is

- b) var'bl principle of elastostatics should achieve its min energy.

Discn of (b) would take us too far afield, so we'll stick to (a). [But let me mention: (b) $\Leftrightarrow$ the elastic energy density is "quasiconvex".]

Essence of (a) is that $F \rightarrow W(F)$ should be (strictly) rank-one convex

$$\sum \frac{\partial^2 W}{\partial F_{i\alpha} \partial F_{j\beta}} \xi_i \xi_j \eta_\alpha \eta_\beta \geq C |\xi|^2 |\eta|^2$$

for all $\xi, \eta \in \mathbb{R}^3$. (Equivalently: restrn of W to a rank-one line $F + t\xi \otimes \eta$ is a convex fn of t .)

Intuition about why this should be needed: ellipticity is assessed by "freezing the coeffs" in the highest-order term, which for div P is $\sum_{\alpha, \beta, i} \frac{\partial^2 W}{\partial F_{i\alpha} \partial F_{j\beta}} \frac{\partial^2 x_j}{\partial x_\alpha \partial x_\beta}$,

so let's discuss the pde

$$\sum_i A_{i\alpha j\beta} \frac{\partial^2 u_i}{\partial x_\alpha \partial x_\beta} = f_i$$

with $A_{i\alpha j\beta}$ constant. If the pde holds in all $\mathbb{R}^n$ then we can use Fourier transform:

$$-\sum_{\alpha, \beta, i} k_\alpha k_\beta A_{i\alpha j\beta} \hat{u}_i(k) = \hat{f}_i(k)$$

The condition

$$\sum_{\alpha, \beta, i, j} A_{i\alpha j\beta} \xi_i \xi_j \gamma_\alpha \gamma_\beta \geq C |\xi|^2 |\gamma|^2$$

asserts that $\sum_{\alpha, \beta} k_\alpha k_\beta A_{i\alpha j\beta}$ (which must be inverted) is positive definite.

Why not just take W to be convex? Well, the set of all rotations $SO(3)$ is not convex. So

W is min at $F \in SO(3)$ [only] $\Rightarrow W$ cannot be convex

More concretely: $\begin{bmatrix} -1 & 0 & 0 \\ 0 & -1 & 0 \\ 0 & 0 & 1 \end{bmatrix} = R_0$ is an orientation-

preserving rotation; but if $W(I) = 0$ + $W(R_0) = 0$ then $W(\frac{1}{2}I + \frac{1}{2}R_0) \leq 0$, yet $\frac{1}{2}I + \frac{1}{2}R_0 = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix}$ isn't even invertible.

Where to look for acceptable W 's?

Fact: if $W(F) = \text{convex fn of } F$
+ convex fn of $\det F$

then W is rank-one convex (indeed, even "quasiconvex").

How to find a frame-indifferent convex fn of F ? Use this result (proved eg as Thm 4.9-1 in Ciarlet's book): if $W(F) = \phi(\lambda_1, \lambda_2, \lambda_3)$ in terms of $\lambda_i = \text{principal stretches}$ (the eigenvalues of $\sqrt{F^T F}$) with ϕ symmetric, convex, and nondecreasing in each variable, then W is a convex fn of F .

A simple (though extreme) case is the "incompressible neoHookean" material

$$W(F) = (\lambda_1^2 + \lambda_2^2 + \lambda_3^2 - 3) \quad \text{restr by } \lambda_1 \lambda_2 \lambda_3 = 1.$$

(Note: $\lambda_1^2 + \lambda_2^2 + \lambda_3^2 = \text{tr}(F^T F) = \sum F_{ix}^2$ is obviously convex!)

There's much more to say about where to find choices of W that are rank-one convex & also frame-indifferent and minimized exactly at the rotations. Ciarlet's chap 4 has a good treatment.

We briefly touched on incompressible elasticity above. In fact rubber and some other polymers are very nearly incompressible so the neo-Hookean law is widely used (at least when the strain is small).

But what does the pde of static equilibrium look like in this case? Short answer: it includes an unknown function - the pressure - as a Lagrange multiplier for the constraint of incompressibility; the constitutive law is in fact

$$\mathbb{T} = -p \mathbb{I} + \tau^*(F)$$

where τ^* is given by an elastic energy

using the methods discussed above (but applied only when $\det F = 1$) and p is determined by balance of forces.

Explain this: starting from constrained variational principle:

$$0 = \delta \int_{\Omega} W(\partial x / \partial X) dX, \quad \det(\partial x / \partial X) = 1$$

by method of Lagrange mult the EL eqn is formally

$$0 = \delta \int_{\Omega} W(\partial x / \partial X) + \gamma(X) [\det(\partial x / \partial X) - 1] dX$$

for some (unknown) $\gamma(X)$. Our task is to show that the Cauchy stress assoc to $\gamma(X) [\det(\partial x / \partial X) - 1]$ has the form $-pI$ for some $p(x)$. The key to this is Cramer's rule, which says

$$\frac{\partial(\det F)}{\partial F_{ix}} = J(F^{-1})^T$$

(Note: LHS is the matrix of minors!)

Recalling that $P = J \mathbb{I} (F^{-1})^T$, ie $\mathbb{I} = J^{-1} P F^T$,

we get

$$P = \gamma \frac{\partial \det F}{\partial F_{ix}} \Rightarrow I = J^{-1} (\gamma J (F^{-1})^T) F^T = \gamma I.$$

so the assertion is proved (with $\gamma(X) = -p(x)$).

Returning to the general (compressible) case, let me mention another viewpoint that's sometimes useful.

I said before that in the isotropic case $W(F) = \phi(\lambda_1, \lambda_2, \lambda_3)$ where λ_i are the principal stretches & ϕ is a symmetric S_n of 3 variables. A different representation of the same set of S_n 's is

$$W(F) = \psi(I, II, III)$$

where I, II, III are the elementary symmetric S_n 's of the eigenvalues of $F^T F = C$, i.e.

$$\begin{aligned} I &= \text{tr } C = \lambda_1^2 + \lambda_2^2 + \lambda_3^2 \\ II &= \frac{1}{2}[(\text{tr } C)^2 - \text{tr } C^2] = \lambda_1^2 \lambda_2^2 + \lambda_1^2 \lambda_3^2 + \lambda_2^2 \lambda_3^2 \\ III &= \det C = \lambda_1^2 \lambda_2^2 \lambda_3^2 \end{aligned}$$

Key advantages of this repr: ψ has no symmetry reqts, and the Piola-Kirchhoff

stress is polynomial expression in terms of Ψ and components of F .

There is an analogous framework for constitutive modeling in Cauchy elasticity:

$$\Sigma(F) = \phi_0 I + \phi_1 B + \phi_2 B^2$$

where $B = FF^T$ and ϕ_i are suitable fns of I, II, III . (Note: $B = FF^T$ and $C = F^T F$ have the same eigenvalues, though their eigenvectors are generally different.) HW3 will ask you to identify ϕ_0, ϕ_1 , and ϕ_2 when $W(F) = \Psi(I, II, III)$.

HW3 will also explore

- how nonlinearities of elasticity explain observable effects like reln b/t pressure & radius when blowing up a (spherical) balloon
- how expts can be used to identify the constitutive law.

(Lecture 6 will start linear elasticity.)