

Calculus of Variations, Lecture 9, 4/2/2013.

We have, up to now, focused largely on var'l pbms that have solutions; though we know from simple examples that lots of var'l pbms don't have solus (for example:  $\min \int_0^1 (u_x^2 - 1)^2 + u^2$ ).

Today: some examples from applications of var'l pbms that "don't have solutions." As in the simplest 1D example (above), minimization in such settings requires "microstructure," and the natural goals are to

- a) identify the favorable microstructures
- b) give an algorithm for constructing minimizing sequences.

We'll achieve both (in some examples) by considering a suitable relaxed variational problem.

My examples today do not come from optimal control, but I note that there are also lots of optimal control problems that require relaxation (cf the book on reserve by Cambridge).

Example 1: thin elastic sheets (reference: AC Pipkin, IMA of Appl Math 36, 1986, pp 85-99)

Consider a thin rubber sheet. To keep things simple, let's use the neo-Hookean model for 3D rubber, i.e. let's assume rubber is incompressible with "elastic energy"

$$W_{3D}(F) = \lambda_1^2 + \lambda_2^2 + \lambda_3^2 - 3$$

where  $\{\lambda_i\}_{i=1}^3$  are the prin stretches (eigenvalues of  $(F^T F)^{1/2}$ ) and  $\lambda_1 \lambda_2 \lambda_3 = 1$  is a constraint.

This is clearly polyconvex, since  $\lambda_1^2 + \lambda_2^2 + \lambda_3^2 = \text{tr}(F^T F)$  is a convex function of  $F$  and  $\det F = 1$  is a polyconvex constraint.

Model a thin sheet by assuming the deformation gradient is constant wr to thickness. Then we can focus on the map  $u: \mathbb{R}^2 \rightarrow \mathbb{R}^3$  taking the (flat) reference sheet to its position in  $\mathbb{R}^3$ .  
Since

$$|Du \cdot v|^2 = \langle Du^T Du v, v \rangle \quad \text{for } v \in \mathbb{R}^2,$$

stretching + compression in-plane are assoc to eigenvalues of  $(Du)^T Du$ : call these  $\lambda_1, \lambda_2$ .

By incompressibility of the 3D sheet, the energy

per unit area (per unit thickness) is then

$$W_{2D} = \lambda_1^2 + \lambda_2^2 + \frac{1}{2\lambda_1\lambda_2} - 3.$$

The var'ial pbm

$$\int_{\Omega} W_{2D}(Dx) \, dx$$

is "in need of relaxation", in the sense that

a)  $\int_{\Omega} W_{2D}(Dx) \, dx$  is not lower semicontinuous

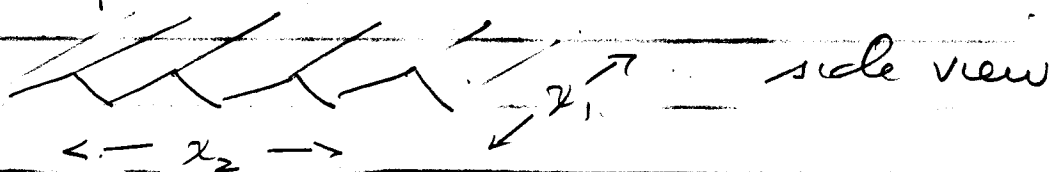
b) for some choices of bc (or lower order terms), this var'ial pbm (or its envelopes with lower order terms) don't achieve their minima.

The key pt: a sheet can avoid compression by wrinkling. If the bc or lower order term requires the wrinkling to be infinitesimal then one gets nonexistence.

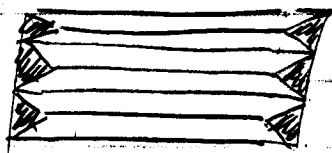
A little detail: consider bc  $u_0 = \begin{bmatrix} 1 & 0 \\ 0 & 1/2 \\ 0 & 0 \end{bmatrix} \cdot \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$  at  $\partial\Omega$ ,

with  $\Omega =$  a square in  $\mathbb{R}^2$ . The sheet could meet the bc using  $u = \begin{bmatrix} 1 & 0 \\ 0 & 1/2 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$  but this involves a

lot of compression. It can achieve energy 0 and almost meet the bc by wrinkling, with wrinkles parallel to the  $x_1$  axis. Making a choice,  $u$  can even be piecewise linear



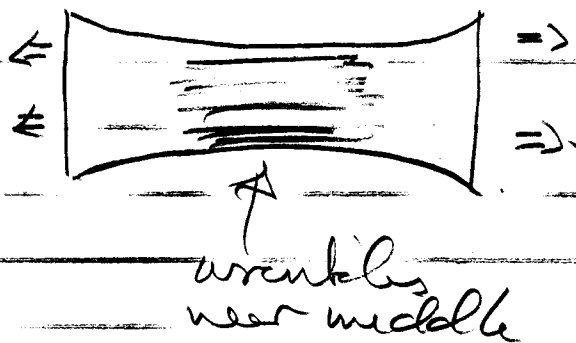
But  $\circ$  a wrinkled det cannot meet the bc. So one needs a bdy layer near the sides where the wrinkles end. The det can still be piecewise linear



If scale of wrinkling is  $\delta$  then bdy layer of width abt  $\delta$  achieves energy  $\sim \delta^2$  while exactly meeting bc.

Even without bdy layer, the wrinkling argt above gives (as  $\delta \rightarrow 0$ ) a counterexample to lsc.

Does this mean thin elastic sheets always wrinkle? Of course not, but they can wrinkle. Classic example (Audoly + Bordenau, PRL 2003): a rectangular sheet, pulled by stiff ruler at 2 opposite sides



Example 2: Optimal designs (one of many pbms addressed by my work with G Strang in the 1980's; for this one see our article "Fibered structures in optimal designs," in Slemmon + Jarvis eds, Theory of Ordinary + Partial Diff'l Eqns, Longman, 1986)

We discussed earlier this semester how to find the smallest  $t_0$  st

$$\exists \sigma, |\sigma| \leq t_0, \operatorname{div} \sigma = 0 \text{ in } \Omega$$

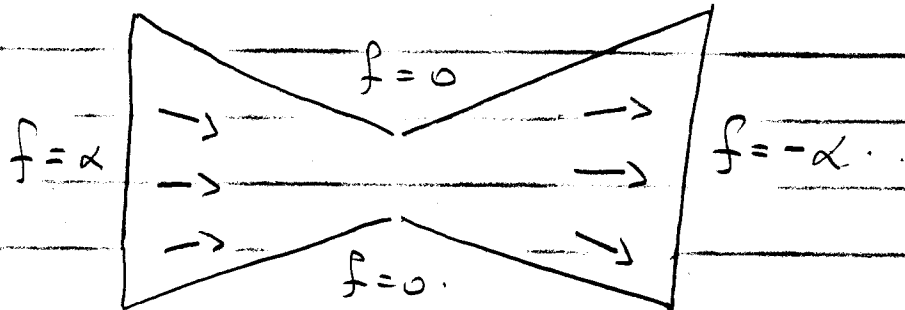
$$\sigma \cdot n = f \text{ at } \partial \Omega$$

where  $f: \partial\Omega \rightarrow \mathbb{R}$  is specified with mean value 0. (Well: we discussed similar problems, and the verbiage we used there can be used here as well.)

Suppose the smallest  $t_0$  is larger than 1 - so there exists  $\sigma$  (probably lots of them) with

$$(*) \quad |\sigma| \leq 1, \quad \text{div} \sigma = 0 \text{ in } \Omega, \\ \sigma \cdot n = f \text{ at } \partial\Omega$$

Example to keep in mind



(neck is a bottleneck for getting stuff from "source" at LHS to "sink" at RHS; need  $\alpha$  sufficiently small for existence of such  $\sigma$ )

[If you don't like thinking about div-free vector fields, question can be reformulated in 2D to

involve gradients since  $\operatorname{div} \sigma = 0 \Leftrightarrow \sigma = (\partial_x u, \partial_y u)$   
 and  $\sigma \cdot n = \partial_{\tan} u$ ; so (\*) is equal to

$$|\nabla u| \leq 1 \text{ in } \Omega, \quad u = F \text{ at } \partial\Omega$$

where  $F = 1^{\text{st}}$  integral of  $f$ .]

OK, here's the question: suppose we'd like to take  $\sigma = 0$  on some subset of  $\Omega$ . How big can this subset be? (If  $\sigma$  represents a flow, we'd like to restrict the flow to a subset of  $\Omega$ ; how much area can we remove?)

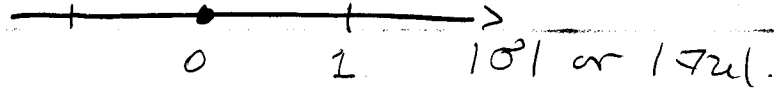
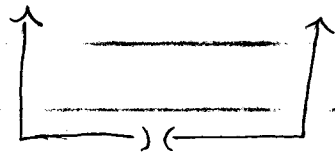
Answer: max area where  $\sigma = 0 \Leftrightarrow$  min area where  $\sigma \neq 0 \Leftrightarrow$

$$\begin{aligned} & \min_{\substack{\operatorname{div} \sigma = 0 \text{ in } \Omega \\ \sigma \cdot n = f \text{ at } \partial\Omega \\ |\sigma| \leq 1 \text{ ptwise}}} \int_{\Omega} \mathbb{1}_{\{\sigma \neq 0\}} \, dx \end{aligned}$$

or equivalently

$$\begin{aligned} & \min_{\substack{u = F \text{ at } \partial\Omega \\ |\nabla u| \leq 1 \text{ ptwise}}} \int_{\Omega} \mathbb{1}_{\{|\nabla u| > 0\}} \, dx \end{aligned}$$

The integrand here is clearly very nonconvex



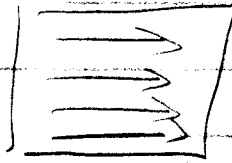
We'll show (perhaps next wk) that the answer involves solving the relaxed (in this case, convexified) problem

$$\min_{\sigma, n=f} \int_{\Omega} |10| \quad \text{or} \quad \min_{u=Fat} \int_{\Omega} |7u|$$

$$|10| \leq 1 \quad |7u| \leq 1$$

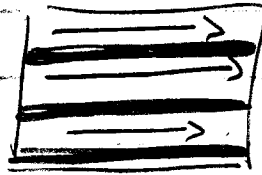
$$\operatorname{div} \sigma = 0$$

Where "relaxed plan" has  $0 < |10| < 1$ , optimal design uses a flow with same direction, but oscillating between 0 + normal 1



uniform  
flow, magnitude  
less than 1

corresp to



holes parallel  
to flow,  $|10|=1$  where  
you keep material.



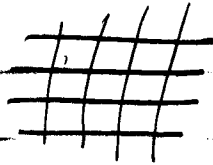
(Remark: The relaxed problem in this example can be solved more or less explicitly, using co-area formula. See R Kohn + G Strang, "The constrained least gradient problem" in Kohn + Lacey eds, *Nonclassical Continuum Mechanics*, CUP 1987, 226-243 + later, more rigorous treatment by Sternberg, Williams, + Zener, *Trans AMS* 339 (1993) 403-432.)

Example 3: Twinning due to martensitic phase transformation. (Reference: book by K. Bhattacharya on *Shape memory materials*; or Ball + James, *Phil Trans: Phys Sci + Eng'g* 338, 1992, 389-450.)

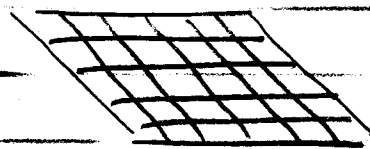
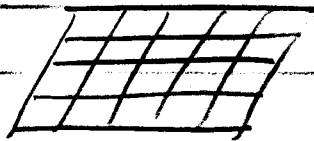
Real phenomenon is 3D but I'll explain in 2D using a "square-to-parallelogram" phase transition.

A "shape memory material" is a crystalline material with a simple (high-symmetry) structure at high temps ( $T > T_c$ ) + several (symmetry-related) possible structures at lower temps ( $T < T_c$ ).

2D version: cubic structure  $T > T_c$



2 phases (neither all = parallelogram)  
for  $T < T_c$



both sheared rel to cubic phase

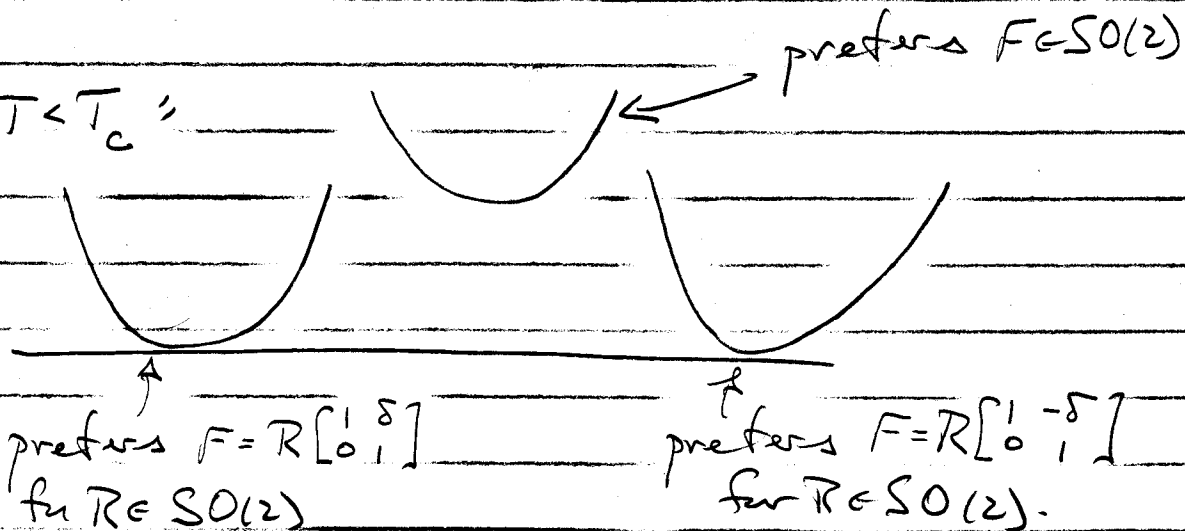
If we ignore issue of nucleation / motion of phase boundaries, we can suppose the material chooses the phase of lowest energy for a given deformation gradient. So

$$E = \int W(F) \quad F = \frac{\partial x}{\partial X}$$

where

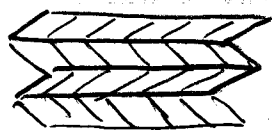
$$W = \min_{i=1,2,3} \{ W_i(F) \}$$

Picture at  $T < T_c$



9.11.

The sheared phases can be mixed in layers



"atomic scale picture"  
assoc piecewise linear &  
cont's deformation  $\chi(X)$   
st  $F = \frac{\partial \chi}{\partial X}$  takes just 2  
values  $\begin{bmatrix} 1 & \delta \\ 0 & 1 \end{bmatrix} + \begin{bmatrix} 1 & -\delta \\ 0 & 1 \end{bmatrix}$

Average  $F$  can be  $\begin{bmatrix} 1 & \lambda \\ 0 & 1 \end{bmatrix}$  for any  $|\lambda| < \delta$ .

Consequence: a region of "parallelogram phase"  
can be surrounded by "square phase" at  
 $T = T_c$  with energy  $\approx 0$ , by using  
infinitesimal layering (as above) with  $\lambda = \frac{1}{2}$ .  
This is what happens.

Another question: what other avg deforms  
can be achieved by mixing deforms in the "wells"  
 $SO(2) \begin{bmatrix} 1 & \delta \\ 0 & 1 \end{bmatrix} + SO(2) \begin{bmatrix} 1 & -\delta \\ 0 & 1 \end{bmatrix}$ , with (presumably)  
more complicated geometry? Answer was  
determined by Ball & James in article  
cited above.

Wrapping around all 3 examples:

9.12

a) when there's a problem with lower semicontinuity, this can often be detected very simply, using piecewise linear det's in a simple "layered" geometry.

[But; not always! - cf Sverak's pt that rank one convexity is not equivalent to quasiconvexity.]

b) applications often lead us to consider energies that are very nonconvex, and definitely not lower semicontinuous.

c) proper goal in such settings is to understand energetically preferred microstructures, and/or to give examples of energy-minimizing sequences.

d) in most settings there are natural "regularizations" that restore existence (eg "bending energy" for thin sheets, or "perimeter" for the optimal design problem).